

Patent 528304

Disclosed is a method of manufacturing a composite product comprising providing a substrate layer and a slurry formulation including a hydraulic binder and dewatering agent. The slurry is then applied to the substrate layer to form a functional layer and the functional layer dewatered through the substrate layer. The application of the slurry to form the functional layer and dewatering steps can be repeated to build up a laminated composite product. Functional additives may be included in each layer to provide desired properties to that layer and indeed to the subsequent composite product.

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TITLE: A COMPOSITE PRODUCT

TECHNICAL FIELD

This application claims priority from the following Australian provisional patent applications, the full contents of which are hereby incorporated by cross-reference.

Application No	Title	Date Filed
PR3474	A Composite Product	2 March 2001
PR3475	Spattering Apparatus	2 March 2001
PR3476	Additive for a Dewaterable Slurry	2 March 2001
PR3477	A Method and Apparatus for Forming a Laminated Sheet Material by Spattering	2 March 2001
PR3478	Coatings for Building Products	2 March 2001

The present invention relates composites and particularly, but not only fibre reinforced building composites.

BACKGROUND ART

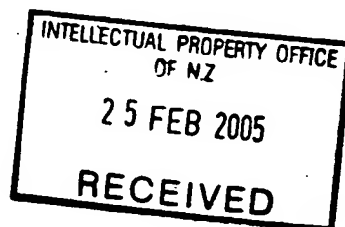
Any discussion of the prior art throughout the specification should in no way be considered as an admission that such prior art is widely known or forms part of common general knowledge in the field.

Fibre reinforced cement is an extremely popular building product.

The applicant along with other various parties have developed a variety of techniques for producing fibre reinforced cement building products and tailoring those FRC products to the particular environment of use.

There are still, however, certain limitations with regard to FRC products. They have limited acoustic, thermal and fire retardant properties. They can exhibit limited workability and generally lie in the medium density range (around 1300kg/m³) or higher (compressed densities of around 1700 kg/m³).

Generally the properties of fibre cement are altered by addition of other materials eg different fibres, fillers etc or altered with different production techniques. Such alterations to the FRC formulation, however, can be expensive to develop in order to ensure no detrimental side effects arise from such new formulations. Alterations in production methods or equipment are also expensive and time consuming to develop. Such techniques also do not provide for true "tailoring" of the FRC product. It is, of



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course, inappropriate to shut down an entire production line, for example, to produce a small batch of FRC product tailored to a specific use.

It is an object of the present invention to overcome or ameliorate at least one of the disadvantages of the prior art, or to provide a useful alternative.

5 DISCLOSURE OF THE INVENTION

In a broad aspect, the present invention provides a composite product comprising a substrate layer and one or more functional layers applied thereto, each functional layer including a mixture of hydraulic binder, dewatering agent wherein the quantity of dewatering agent is sufficient to permit de-watering of each functional layer through the
10 substrate layer and any additional functional layer.

In a second aspect, the present invention provides a method of manufacturing a composite product comprising:

- (i) providing a substrate layer,
- (ii) providing a slurry formulation including an hydraulic binder and dewatering
15 agent,
- (iii) applying said slurry to said substrate layer to form a functional layer,
- (iv) dewatering the functional layer, and
- (v) optionally repeating steps (ii) through (iv), wherein the quantity of dewatering agent is sufficient to maintain porosity and thereby permit de-watering of each functional layer
20 through the substrate layer and any additional functional layer.

Preferably, the substrate layer is a fibre reinforced base material such as fibre reinforced cement. This substrate layer provides a structural base on which additional functional layers may be added:

The functional layers may be added to both sides of the substrate layer but most
25 preferably are added to one side which generally expose one side of the building board during production. Such a technique allows the aforementioned method to be applied to current FRC production techniques Hatschek.

The present applicants have developed a process for manufacture of a composite article to virtually any desired specification or use. To explain, the present inventive
30 composite and method starts with a simple water permeable substrate layer such as conventional fibre reinforced building board. To this base layer are added one or more functional layers, each functional layer being specifically tailored to provide the desired

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functionality. For example, if it is desired to provide an insulating layer, the slurry formulation from which the functional layer is formed can include insulating materials such as rubber crumbs, vermiculite, perlite, gypsum, etc.

Similarly, water permeability may be decreased by including water resistant
5 polymers eg silanes, siloxane blends etc or pozzalanic materials such as silica fume, metakaoline, ultrafine fly ash etc.

Density modification of the functional layer can be accomplished by addition of suitable light weight materials such as cenospheres (ceramic hollow spheres), expanded polystyrene, vermiculite, perlite etc.

10 The inventive process enables various functional layers to be integrated into a single composite by appropriate slurry modification.

In a preferred embodiment, each functional layer has a reinforcing layer positioned therebetween. The reinforcing layer may comprise fibre mesh or netting, and serves to improve the strength and durability of the composite product.

15 In some instances, the reinforcing layer may comprise a thin fibre reinforced cementitious layer similar for instance to the base material. This provides for more efficient utilisation of such fibre reinforced layers, similar to sandwich composite technology. It will be appreciated by a person skilled in the art, that there are areas of a composite which require less fibre reinforcement ie the core. Such a core area can be
20 formed as the aforementioned functional layer with low fibre reinforcement. Areas which require high fibre reinforcement due to high tensile strength ie surface or skin areas, can be covered by a fibre reinforced cementitious layer. The thus formed fibre reinforced layers act as sandwich skins with a de-watered slurry functional layer acting as a sandwich core.

25 As a result, the described composite provides significant advantages over monolithic fibre reinforced composites. Firstly, by the aforementioned composite action, fibres can be positioned in areas where they are most required. This will, of course, lead to a reduction in the fibre reinforced volume of the product.

Secondly, such a reduced fibre volume will lead to an improvement in non-
30 combustibility and thermal insulation performance of the composite. Production of a non-combustible composite has, in the past, been difficult to achieve due the high cost of non-combustible fibres and specialised processes required for their use.

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Further, one of the most important advantages arising from the present invention is the ability to concentrate a particular functionality into a single layer. To explain, in large monolithic structural layers, particularly fibre reinforced cement building products, any adjustments to the functional or structural aspects of the product, can be diluted or diminished or unevenly spread throughout the product. There is also the possibility of adverse side reactions occurring during production of such a monolithic product which may diminish the structural or functional attributes required. With the present invention, on the other hand, it is possible to concentrate or target specific functional or structural attributes within a single functional layer thereby assuring the attribute is provided to the resultant composite product.

Indeed, various optional additives and filler can be incorporated for specific purposes, ie acoustic, thermal or fire performance, density modification, cost or production efficiency.

A top or finish coating layer can also be provided for the composite product by a fibre reinforced cementitious layer, a material similar or identical to the functional layer or any other product. In one particularly preferred embodiment, the top or finishing coating can be primarily an "aesthetic" layer of, say, ultrafine particle size or made from a sandable material to smooth the exterior surface of the composite product and thereby provide a finish/paint ready surface.

Unless the context clearly requires otherwise, throughout the description and the claims, the words 'comprise', 'comprising', and the like are to be construed in an inclusive sense as opposed to an exclusive or exhaustive sense; that is to say, in the sense of "including, but not limited to".

The dewatering agent serves to maintain sufficient porosity in the slurry and product to be coated to permit dewatering of the slurry through the product to be coated. Preferably, the dewatering agent is a particulate material such as fly ash, alumina trihydrate, silica flour, cenospheres (ceramic hollow spheres) or similar.

Fly ash is particularly preferred as it permits dewatering of the slurry within a few minutes. Other particulate dewatering agents such as alumina trihydrate or silica flour may also be used, however, they increase the time required for dewatering of the slurry through the product to be coated.

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In a preferred embodiment, the slurry applied to the product to be coated has a high water content. Preferably, the water content can be up to 50%. This is in contrast to previous cementitious formulations which generally have a very high solids content.

By combining the various components of the formulation described above, a self
5 levelling dewaterable slurry is obtained which can be applied to the substrate layer, dewatered through the substrate layer and thereby provide a uniform coating over this substrate layer.

Normally, after application of the coating, the resultant product would be normally cured, steam cured or hydrothermally cured, ie autoclaved, and if required, sanded to a
10 smooth flat finish.

The substrate layer to which the functional layers can be applied is virtually limitless provided the slurry can be dewatered through the substrate layer. Cementitious and gypsum building boards are typical examples of suitable building products on which the coating can be applied.

15 The thickness of the functional layers would range from around 0.1 to 10 mm, preferably 0.5 to 5 mm and most preferably 1 to 3 mm.

After optional sanding, the layer may have a depth of around 0.05 to 5 mm, preferably 1 to 2 mm and most preferably 0.5 to 1 mm. The thus produced composite is comparable in its workability to monolithic (single layer) composites. It can be flexed,
20 cut, drilled and fixed by nails etc to a frame without surface cracking or chipping.

The applicant's have found an extremely good interlaminar bond and compatibility between the dewatered slurry layer and base layer resulting in excellent composite action, compatibility and resistance to delamination.

The term 'hydraulic binder' as used throughout the specification refers to a
25 pulverised material in the solid, dry state which, when mixed with water, yields plastic mixtures that are able to set and harden, for example a cement. Included within the definition are white, grey or pigmented cements and hydraulic limes.

The term 'cement' includes hydraulic and alite cements such as portland cement, blended cements such as portland cement blended with fly ash, blast-furnace slag,
30 pozzalans and the like and mixtures thereof, masonry cement, oil well cement, natural cement, alumina cement, expansive cements and the like, or mixtures thereof.

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The quantity of binder in the formulation is preferably between 10 to 50 wt% based on the total dry ingredients, more preferably 15 to 40 wt% and most preferably 20 to 30 wt%.

The fly ash used in the present invention provides a number of advantages including, particularly, as an aid to dewatering of the slurry as defined above.

The term 'fly ash' as used herein refers to a solid powder having a chemical composition similar to or the same as the composition of material that is produced during combustion of powdered coal, ie 25 to 60 wt% silica, 10 to 30 wt% Al_2O_3 , 5 to 25 wt% Fe_2O_3 , 0 to 20 wt% CaO and 0 to 5 wt% MgO.

In another preferred embodiment, the dewatering agent may include a coarse fraction fly ash which is greater than 100 microns. This coarse fraction fly ash includes bottom ash or similar products from coal combustion. There is an advantage to using these products over the aforementioned particle size fly ash since it is cheaper. Of course, as will be clear to persons skilled in the art, some reformulation of the slurry may be required to provide a suitable coating and appropriate dewatering characteristics when the dewatering agent is such a coarse fraction fly ash.

Fly ash particles are typically spherical and range in diameter from 1 to 100 microns. In a preferred embodiment, the fly ash comprises two components. A first 'larger' size particles of fly ash with preferably a 100 micron maximum size. This size range of fly ash is used in the slurry to aid in improving the dewatering characteristics of the slurry but also as a moderately reactive pozzolan.

The second 'smaller' fly ash size zone which preferably has a 10 micron maximum size also adds an improving dewatering characteristic but is a more highly reactive pozzolan. This 'smaller' fly ash particle zone also improves the sanded surface quality of the finish layer.

In a preferred embodiment, the first fly ash comprises 10 to 60 wt% of the formulation based on total dry ingredients, more preferably 20 to 50 wt% and most preferably 30 to 40 wt%.

The second fly ash component preferably provides 5 to 30 wt% of the formulation based on total dry ingredients, more preferably 10 to 25 wt% and most preferably 15 to 20%.

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The functional layers may optionally contain other additives such as fillers. Such fillers may also be used to improve the dewatering characteristics of the slurry. For example, cenospheres (hollow ceramic microspheres) diatomite, wollastonite, ground rice hulls, ground perlite or the like, are particularly suitable for this purpose.

5 These and other fillers may also be used to provide additional benefits, for example calcium carbonates or alumina hydrates improve sandability and flexibility of the coated layer respectively. Silica flour improves hardness of the sanded surface of the coating layer and the acoustic/thermal insulation properties of the layer can be improved by including rubber particles, vermiculite, perlite, shredded or expanded polystyrene or
10 gypsum.

The fillers preferably comprise 5 to 30 wt% of the formulation based on total dry ingredients, more preferably 10 to 25 wt% and most preferably 25 to 20 wt%.

The functional layers may also contain other organic additives. Cement plasticising agents, for example, may be used to alter the rheology of the slurry. Suitable
15 cement plasticising agents include melamine sulphonate formaldehyde condensates, naphthalene sulphonate formaldehyde condensates, naphthalene sulphonates, calcium lignosulphonates, sodium lignosulphonates, saccharose, sodium gluconate, sulphonic acids, carbohydrates, amino carboxylic acids, polyhydroxycarboxylic acids, sulphonated melomine and the like.

20 The amount of cement plasticiser of course will depend upon the fluidising ability of the particular plasticisers. Generally the quantity of plasticiser will be in the range of 0.3 to about 3 wt% and more preferably 0.5 to 2 wt% based on the total of dry ingredients in the formulation.

Particularly preferred cement plasticisers are Melment F-10, a melamine
25 formaldehyde sodium bisulphate polymer dispersant marketed by SKW-Trostburg in the form of a fine white powder. Another suitable plasticiser is Neosyn, a condensed sodium salt of sulphonated naphthalene formaldehyde available from Hodgson Chemicals.

Another preferred component in the coating is a biopolymer which acts to enhance
30 the flowability, segregation resistance and self levelling qualities of the cementitious slurry. Particularly suitable biopolymers are xanthan gum and/or whelan gum, eg KELCO-CRETE, K1C 376 manufactured by Monsanto.

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Latex may also be included in the formulation to improve adherence, elasticity, stability and impermeability of the functional layers. The latex also improves flexibility of the formed composite.

The latex may be selected from the group consisting of acrylic latex, styrene latex, butadiene latex or mixtures thereof and is provided preferably in an amount between 0.5 to 20%, more preferably 1 to 15% and most preferably about 10% by weight of cement (on polymer solids basis) solids.

Vinyl polymers may also be incorporated into the formulation either in addition or as a substitute to the latex emulsions. Such vinyl polymers or equivalent polymeric materials enhance adhesion, resilience and flexural strength and abrasion resistance of the functional layer.

Preferred vinyl polymers include polyvinyl acetate or a copolymer vinyl acetate with another monomer such as ethylene. A particularly preferred vinyl acetate resin is VINNAPAS LL5044 thermo plastic resin powder which contains a vinyl acetate-ethylene copolymer available from Wacker. Such powdered vinyl polymer is preferably provided in quantities similar to the latex emulsion referred to above.

In addition to the above, conventional other additives such as mineral oxides, hydroxides and clays, metal oxides and hydroxides, fire retardants such as magnesite, thickeners, silica fume or amorphous silica, water sealing agents, water reducing agents, setting modifiers, hardeners, dispersants, foaming agents or flocculating agents, waterproofing agents and density modifiers are suitable for use with the present invention.

In this regard, one particular advantage arising from the present invention is the ability to treat the product to be coated by providing additives in the functional layer. To explain, since the slurry is dewatered through the product to be coated, it is possible to provide additives to the base layer by incorporation in the slurry. For instance, a waterproofing agent such as silane may be included in the formulation in excess of the functional layer requirements. During dewatering, the silane will be drawn into and through the base layer being coated thereby treating the base layer. This simultaneous treatment of the base layer as well as providing a functional attribute via the deposited layer is a valuable additional benefit arising from the aforescribed method.

Best Mode for Carrying Out the Invention

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The present invention will now be described by way of example only with reference to the following embodiments.

In each of the following examples, the product was produced as follows.

Step 1 Slurry preparation

- 5 A slurry of the formulation is prepared by mixing the hydraulic binder, fly ash and other optional components with water. The solids content in the slurry is preferably between 50 and 90%, more preferably 55 to 80% and most preferably 60 to 70%.

Step 2 Slurry application/dewatering

- 10 The slurry is applied to the base layer by any convenient means such as brushes rollers, knives or sprays etc. The slurry is designed to self level and form a uniform coating on the product. The building product to be coated exhibits a certain degree of porosity causing the slurry to dewater and form a uniform deposited cementitious layer. Time for dewatering can vary quite dramatically but normally occurs between 10 and 90 seconds, depending on the porosity of the material to be coated, its water content and 15 thickness and viscosity of the slurry formulation. A vacuum may be used to reduce the slurry dewatering time if required. This is particularly useful when tailoring the coating process to the speed of a building product forming process, eg between 40 to 45 seconds on a Hatschek production line.

Step 3 Curing

- 20 After forming, the green laminate article comprising the building product plus coating is preferably precured for a short time, eg up to 48 hours, then cured by air/moist curing at room temperature, steam curing between 40 and 90°C or autoclaving in a steam pressure vessel between 120 and 200°C.

- For either of these three curing techniques, a curing time range between 6 and 72 25 hours, preferably up to 48 hours, is suitable. Of course, as will be clear to persons skilled in the art, the length of time chosen for curing is dependent on the formulation, the manufacturing process and form of the article.

The following examples relate to specific formulation compositions.

Example 1: Sandable Dewatered Slurry Composition

- 30 Function: sandable, durable finishing layer for façade applications.

The low viscosity slurry (drainage time in 50 ml volume funnel = 3.4 seconds) was applied on the base layer (Hardiform™ 12 mm thick cellulose fibre reinforced cement-

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based green sheet manufactured by James Hardie Industries). The slurry dewatered in 90 seconds (un-aided by vacuum) forming a 1.25 mm thick coating. The coated sheet was autoclave-cured for 8 hrs at 180 °C temperature and 0.80 MPa pressure. It was then sanded flat to 0.60 mm thick using industrial sanders equipped with 100 grit sand paper

5 belts.

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Slurry Composition	% by total weight of solids (S)	Weight in gm
Dewatered Cementitious Composition		
Portland Cement	30	12000
Silica Flour (400 G grade)	10	4000
Fly ash (larger size fraction)	40	16000
Fly ash (smaller size fraction)	20	8000
Total	100	40000
Water (W)		14000
Water/ Solids (W/S ratio)	0.35	
Solids Content (W/W+S)	0.74	
Organic Additives		
Welan Gum (Kelcocrete)	0.0075	3.0
naphthalene formaldehyde Plasticising Agent (Neosyn)	0.25	100.0
Acrylic Emulsion Rhoplex MC1934	1.0	400.0

Example 2: Rubberised Dewatered Slurry Composition

Function: In skid-resistant flooring, hard wearing static dissipative flooring and acoustic insulating ceiling panels.

The low viscosity slurry (drainage time in 50 ml volume funnel = 4.2 seconds) was applied on the base layer (Hardiform™ 12 mm thick cellulose fibre reinforced cement-based green sheet manufactured by James Hardie Industries). The slurry dewatered in 60 seconds (un-aided by vacuum) forming a 1.25 mm thick coating. The coated sheet was autoclave-cured for 8 hrs at 180 °C temperature and 0.80 MPa pressure. It was then sanded flat to 0.60 mm thick using industrial sanders equipped with 100 grit sand paper belts.

Slurry Composition	% by total weight of solids (S)	Weight in gm
Dewatered Cementitious Composition		
Portland Cement	30	12000
Recycled Rubber crumbs (minus 30 mesh)	10	4000
Fly ash (larger size fraction)	40	16000
Fly ash (smaller size fraction)	20	8000
Total	100	40000
Water		13000
Water/ Solids (W/S ratio)	0.325	
Solids Content (W/W+S)	0.755	
Organic Additives		
Welan Gum (Kelcocrete)	0.0075	3.0
naphthalene formaldehyde Plasticising Agent (Neosyn)	0.25	100.0
Acrylic Emulsion Rhoplex MC1934	1.0	400.0

Example 3: Flexible & Sandable Dewatered Slurry Composition

- 5 **Function:** Flexible & sandable layer on thin fibre cement reinforced cement-based lining.

The low viscosity slurry (drainage time in 50 ml volume funnel = 2.8 seconds) was applied on the base layer (Hardiflex™ 4.5 mm thick cellulose fibre reinforced cement-based green sheet manufactured by James Hardie Industries). The slurry
10 dewatered in 120 seconds (un-aided by vacuum) forming a 1.25 mm thick coating. The coated sheet was precured for 48 hours then was autoclave-cured for 8 hrs at 180 °C temperature and 0.80 MPa pressure. It was then sanded flat to 0.60 mm thick using industrial sanders equipped with 100 grit sand paper belts.

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Slurry Composition	% by total weight of solids (S)	Weight in gm
Dewatered Cementitious Composition		
Portland Cement	20	8000
Calcium Carbonate Grade 10 (40um avg. size)	10	4000
Alumina Tri-hydrate (80 um avg. size)	5	2000
Fly ash (larger size fraction)	45	18000
Fly ash (smaller size fraction)	20	8000
Total	100	40000
Water		12000
Water/ Solids (W/S ratio)	0.30	
Solids Content (W/W+S)	0.77	
Organic Additive		
Welan Gum (Kelcocrete)	0.0075	3.0
naphthalene formaldehyde Plasticising Agent (Neosyn)	0.25	100.0
Styrene Acrylic Latex Emulsion (56% solids)	5	2000

Example 4: Flexible & Sandable Dewatered Slurry Composition (Low Cement)**Function:** Flexible & sandable layer on thin fibre cement reinforced

5 cement-based lining.

The low viscosity slurry (drainage time in 50 ml volume funnel = 4.5 seconds) was applied on the base layer (Hardiflex™ 4.5 mm thick cellulose fibre reinforced cement-based green sheet manufactured by James Hardie Industries). The slurry dewatered in 90 seconds (un-aided by vacuum) forming a 1.25 mm thick coating. The coated sheet was

10 autoclave-cured for 8 hrs at 180 °C temperature and 0.80 MPa pressure. It was then sanded flat to 0.60 mm thick using industrial sanders equipped with 100 grit sand paper belts.

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Slurry Composition	% by total weight of solids (S)	Weight in gm
Dewatered Cementitious Composition		
Portland Cement	10	4000
Calcium Carbonate Grade 10 (40um avg. size)	20	8000
Alumina Tri-hydrate (80 um avg. size)	5	2000
Fly ash (larger size fraction)	40	18000
Fly ash (smaller size fraction)	25	10000
Total	100	40000
Water		16000
Water/ Solids (W/S ratio)	0.40	
Solids Content (W/W+S)	0.715	
Organic Additives		
Welan Gum (Kelcocrete)	0.0075	3.0
naphthalene formaldehyde Plasticising Agent (Neosyn)	0.25	100.0
Vinyl acetate-ethylene powdered copolymer (Vinnapas LL5004)	1.625	650

The aforementioned examples provide a composite comparable in workability to monolithic or single layer composites. They can be flexed, cut, drilled or fixed by nails
5 or the like to a frame without surface cracking or chipping.

The surface is 'finish-ready' and remains smooth, flat, crack-free and with low permeability even when used in a curved configuration.

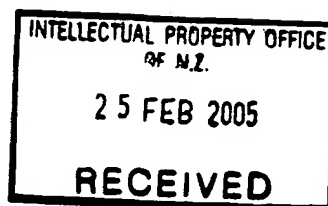
Each example provided excellent interlaminar bond between the base sheet and coating exhibiting good composite action, compatibility and resistance to delamination.

10 The Applicant's have developed a unique process which allows them to combine fibre reinforced layers with functional dewatered slurry layers optional reinforced with a wide range of synthetic or natural fibres, eg polypropylene, glass, PVA, cellulose fibres etc. The outcome of the aforementioned method is to produce a fibre reinforced

composite with strength, water resistance, incombustibility of fibre cement with a low density, surface finish and insulation properties of, for example, gypsum board.

The Applicant's have found that using the techniques described herein, functional layers can be added to the substrate layer with no delamination or incompatibility between the layers, ie no differential shrinking, warping or similar properties.

It will be understood by persons skilled in the art that the present invention may be embodied in other forms without departing from the scope of the inventive idea as described herein. In particular, it will be appreciated that the formulations, coatings, additives, methods and composite products of the present invention are suitable or may be adapted for use in conjunction with the methods and apparatus as described in the various priority documents.



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CLAIMS:

1. A composite product comprising a substrate layer and one or more functional layers applied thereto, each functional layer including a mixture of hydraulic binder, dewatering agent wherein the quantity of dewatering agent is sufficient to permit de-
5 watering of each functional layer through the substrate layer and any additional functional layer.
2. A composite product according to claim 1, wherein each functional layer includes one or more functional additives to provide desired properties to that layer.
3. A composite product according to claim 1 or claim 2, wherein the substrate layer
10 is a fibre reinforced base material.
4. A composite product according to any one of the preceding claims, wherein the substrate layer is a reinforced cementitious product.
5. A composite product according to any one of the preceding claims, wherein the functional layers are added to both sides of the substrate layer.
- 15 6. A composite product according to any one of the preceding claims, wherein the functional layers are added to one side of the substrate layer.
7. A composite product according to any one of the preceding claims, wherein each functional layer is covered by a reinforcing layer.
8. A composite product according to any one of the preceding claims, wherein the
20 reinforcing layer comprises fibre mesh or netting.
9. A composite product according to any one of the preceding claims, wherein the reinforcing layer is a fibre reinforced cementitious layer.
10. A composite product according to any one of the preceding claims, wherein the composite product comprises outer layers provided by fibre reinforced cementitious
25 layers with one or more functional layers positioned therebetween.
11. A composite product according to any one of the preceding claims, wherein the functional layers have a low fibre content relative to the fibre reinforced cementitious layers.
12. A composite product according to any one of the preceding claims, wherein
30 additives and/or fillers are incorporated in the functional layers to provide the desired acoustic properties, thermal or fire performance, density modification, cost or production

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efficiency, compressive or tensile strength, water permeability, density or aesthetic properties to the composite product.

13. A composite product according to any one of the preceding claims, wherein the dewatering agent is provided in a sufficient quantity to maintain porosity functional layer(s) and the substrate layer during dewatering.
14. A composite product according to any one of the preceding claims, wherein the dewatering agent is a particulate material.
15. A composite product according to any one of the preceding claims, wherein the dewatering agent is selected from fly ash, alumina trihydrate, silica flour, cenospheres or mixtures thereof.
16. A composite product according to any one of the preceding claims, wherein, after coating, the coated product is cured by air curing, steam curing or hydrothermally cured in an autoclave.
17. A composite product according to any one of the preceding claims, wherein the product to be coated is cementitious building board or product or gypsum building board.
18. A composite product according to any one of the preceding claims, wherein the thickness of the functional layer on the product is between 0.1 and 10 mm.
19. A composite product according to any one of the preceding claims, wherein the hydraulic binder used in the coating is selected from the group consisting of white, grey or pigmented cements, hydraulic limes or mixtures thereof.
20. A composite product according to any one of the preceding claims, wherein the binder in the formulation is between 10 and 50 wt% based on total dry ingredients.
21. A composite product according to any one of the preceding claims, wherein fly ash is the dewatering agent.
22. A composite product according to any one of the preceding claims, wherein the dewatering agent comprises:
 - i) 10 to 60% of the formulation based on total dry ingredients of a first fly ash component having a particle diameter between 1 and 100 microns; and
 - ii) 5 to 30 wt% of the formulation based on total dry ingredients of a second fly ash component having a maximum particle size diameter of around 10 microns.

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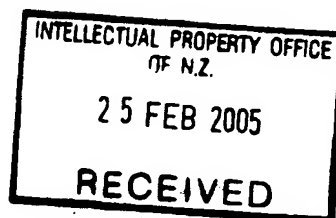
23. A composite product according to any one of the preceding claims, wherein the dewatering agent includes a coarse fraction fly ash having a particle size diameter greater than 100 microns.
24. A composite product according to any one of the preceding claims, wherein the
5 functional layer includes additives to improve the properties of the substrate layer such that upon dewatering of the functional layer, the substrate layer is thus treated with said additive.
25. A method of manufacturing a composite product comprising:
(i) providing a substrate layer,
10 (ii) providing a slurry formulation including an hydraulic binder and dewatering agent,
(iii) applying said slurry to said substrate layer to form a functional layer,
(iv) dewatering the functional layer, and
(v) optionally repeating steps (ii) through (iv), wherein the quantity of dewatering
15 agent is sufficient to maintain porosity and thereby permit de-watering of each functional layer through the substrate layer and any additional functional layer.
26. A method according to claim 25, wherein each functional layer includes one or more functional additives to provide desired properties to that layer.
27. A method according to claim 25 or claim 26, wherein the substrate layer is a fibre
20 reinforced base material.
28. A method according to any one of claims 25 to 27, wherein the substrate layer is a reinforced cementitious product.
29. A method according to any one of claims 25 to 28, wherein the functional layers are added to both sides of the substrate layer.
- 25 30. A method according to any one of claims 25 to 29, wherein the functional layers are added to one side of the substrate layer.
31. A method according to any one of claims 25 to 30, wherein each functional layer includes one or more functional additives to provide desired properties to that layer.
32. A method according to any one of claims 25 to 31, wherein each functional layer
30 is covered by a reinforcing layer.
33. A method according to any one of claims 25 to 32, wherein the reinforcing layer comprises fibre mesh or netting.

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34. A method according to any one of claims 25 to 33, wherein the reinforcing layer is a fibre reinforced cementitious layer.
35. A method according to any one of claims 25 to 34, wherein the composite product comprises outer layers provided by fibre reinforced cementitious layers with one
5 or more functional layers positioned therebetween.
36. A method according to any one of claims 25 to 35, wherein the functional layers have a low fibre content relative to the fibre reinforced cementitious layers.
37. A method according to any one of claims 25 to 36, wherein additives and/or
10 fillers are incorporated in the functional layers to provide the desired acoustic properties, thermal or fire performance, density modification, cost or production efficiency, compressive or tensile strength, water permeability, density or aesthetic properties to the composite product.
38. A method according to any one of claims 25 to 37, wherein the dewatering agent is provided in a sufficient quantity to maintain porosity in the functional layers and the
15 substrate layer during dewatering.
39. A method according to any one of claims 25 to 38, wherein the dewatering agent is a particulate material.
40. A method according to any one of claims 25 to 39, wherein the dewatering agent is selected from fly ash, alumina trihydrate, silica flour, cenospheres or mixtures thereof.
- 20 41. A method according to any one of claims 25 to 40, wherein, after coating, the coated product is cured by air curing, steam curing or hydrothermally cured in an autoclave.
42. A method according to any one of claims 25 to 41, wherein the product to be coated is cementitious building board or product or gypsum building board.
- 25 43. A method according to any one of claims 25 to 42, wherein the thickness of the functional layer on the product is between 0.1 and 10 mm.
44. A method according to any one of claims 25 to 43, wherein the hydraulic binder used in the coating is selected from the group consisting of white, grey or pigmented cements, hydraulic limes or mixtures thereof.
- 30 45. A method according to any one of claims 25 to 44, wherein the binder in the formulation is between 10 and 50 wt% based on total dry ingredients.

46. A method according to any one of claims 25 to 45, wherein fly ash is the dewatering agent.
47. A method according to any one of claims 25 to 46, wherein the dewatering agent comprises:
- i) 10 to 60% of the formulation based on total dry ingredients of a first fly ash component having a particle diameter between 1 and 100 microns; and
 - ii) 5 to 30 wt% of the formulation based on total dry ingredients of a second fly ash component having a maximum particle size diameter of around 10 microns.
48. A method according to any one of claims 25 to 47, wherein the dewatering agent includes a coarse fraction fly ash having a particle size diameter greater than 100 microns.
49. A method according to any one of claims 25 to 48, wherein the functional layer includes additives to improve the properties of the substrate layer such that upon dewatering of the functional layer, the substrate layer is thus treated with said additive.
50. A method according to any one of claims 25 to 49, wherein the slurry formulation is applied to the substrate layer by means of splattering.
51. A composite product according to any one of claims 1 to 24, substantially as herein described with reference to examples 1-4.
52. A composite product, substantially as herein described with reference to examples 1-4.
53. A method according to any one of claims 25 to 50, substantially as herein described with reference to examples 1-4.
54. A method for manufacturing a composite product, substantially as herein described with reference to examples 1-4.

END OF CLAIMS



END